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Determination of moment, shear and ductility capacities of spiral columns using an artificial neural network



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ABSTRACT

Intelligent systems are frequently used to solve difficult and complex problems in today's world. Especially in the discipline of civil engineering, much research has been conducted with the help of intelligent systems. The objective of this study is to identify the moment and shear force capacities of reinforced concrete spiral columns and their displacement ductility values by using an algorithm based on an Artificial Neural Network (ANN). In the study, 86 different spiral column experiments tested in the literature were compiled, and the moment and shear force capacities obtained through the experiments were arranged at a certain level. In addition, the ductility values of the tested columns were calculated using graphical experimental data. The output layer consists of four neural network models, which are ANN₁ (with three output neurons), ANN₂, ANN₃, and ANN₄ (with one output neuron), and moment, shear force capacity, and displacement ductility parameters were obtained, respectively. According to results of this study, it was observed that moment and shear force capacities of spiral columns could be particularly well estimated using ANN. However, it was found that the estimation success of ANN for displacement ductility was not sufficient.

1. Introduction

Columns are known as the most important load-bearing elements of reinforced concrete buildings. The damage inflicted by an earthquake on one of these elements affects the whole structure and the building collapses when the damage increases. These bearing elements cannot be exposed to only axial load due to a casting feature of reinforced concrete constructions. Therefore, the columns reach their load-bearing capacity under section effect while bearing moment and shear force capacity in addition to axial load under vertical and horizontal loads. When one of these section impacts exceeds the ultimate capacity, the column reaches ultimate capacity and the behavior of the column is determined with respect to this parameter.

The failure as a result of exceeding the moment capacity of columns due to increased horizontal load during an earthquake is a desired behavioral model. It is because while a rotation occurs in the section under a fixed normal force value in critical section areas where plastic hinges are formed due to the force of the earthquake, ductile section behavior is formed without a significant change in achieved moment value.

The shear force has critical effect on reinforced concrete columns which are exposed to horizontal load during an earthquake. Shear force in reinforced concrete columns reduces the horizontal resistance of

buildings and leads to a rapid loss of capacity [1]. Most of the reinforced concrete columns in the past earthquakes have collapsed due to insufficient shear resistance. Therefore, estimating the shear capacity of reinforced concrete columns is of great importance [2].

In terms of seismic performance, it is crucial to provide sufficient ductility in load-bearing systems of buildings or in elements constituting the load-bearing system. It has been widely accepted that in all earthquake regulations it is necessary to provide sufficient ductility level of the elements that form the load-bearing system and particularly the columns. Ductility is a sectional feature that can be measured [3]. The ratios of transverse and longitudinal reinforcement, the presence of confinement, the strength of concrete and reinforcement, and axial forces on the section have a one-to-one impact on ductility values. In order to determine the ductility value of load-bearing system element, displacement and curvature values at yielding and ultimate strength (depletion of power) are needed. In compliance with the capacity design, the ductility of elements should not decrease below certain limit values.

Intelligent systems are frequently used to solve difficult and complex problems in today's world. Especially in the discipline of civil engineering, much research has been conducted with the help of intelligent systems [4–8]. The principal reason for an ANN to be the subject of studies conducted in the field of civil engineering and other

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Abbreviation list

| | |
|---------------|---|
| γ | coefficient reflecting impact of the axial load on the cracking |
| A_{cc} | cross-sectional area of the column |
| A_{si} | sum of cross-section areas of longitudinal reinforcement |
| f_c | compressive strength of the concrete |
| M_r | moment capacity |
| N_r | axial force capacity |
| x_i | distance of column reinforcement to center |
| x_p | distance of column center |
| σ_{si} | reinforcement stress |
| A_c | cross-sectional area of the column |
| A_g | a gross cross-sectional area of the column |
| A_{sw} | sum of cross-section areas of confinement reinforcement |
| A_v | transverse reinforcement area |
| b | column width |
| b_w | column width |
| d | effective depth of column |
| f_c' | compressive strength of the concrete |
| f_{ct} | tensile strength of the concrete |

| | |
|----------------|--|
| f_y | yield strength of circular stirrup or spiral reinforcement |
| f_{yw} | yield strength of confinement reinforcement |
| m | number of test data |
| n | number of elements in the output layer of ANN |
| N_d | the design axial load of the column |
| O | estimated value |
| P | number of test data |
| P | axial load |
| s | the spacing of transverse reinforcement |
| $T_{estimate}$ | estimated values |
| t_i | target value |
| T_{real} | real values |
| V_r | shear force capacity |
| x' | normalized value |
| x_i | input value |
| x_{max} | highest values in the input set |
| x_{min} | lowest values in the input set |
| $y^{(t)}$ | error term |
| L | column effective length |
| ρ_s | volumetric reinforcement ratio (%) |

disciplines is the fact that it offer an alternative solution model for problems which are hard to solve with traditional techniques thanks to its success in approaching and defining the data in different structures and forms.

The objective of this study is to identify moment and shear force capacities and displacement ductility of spiral columns with different engineering features by using an ANN technique, comparing the obtained results with results of laboratory studies and testing the effectiveness of ANN in this field based on the analyses. There was no implementation of smart systems that determine shear, flexural and ductility of spiral columns simultaneously and separately in the literature. The dataset used within the scope of the study was composed of results of 86 spiral column tests obtained from the data bank that includes tests conducted by different researchers at the Pacific Earthquake Engineering Research Center (PEER) and in the literature. 50 of these data sets are used for training, 29 for testing, and 7 for verification. Moment and shear force capacities of columns contained in verification set were compared with theoretical results obtained from current reinforced concrete regulations [9,10] and effectiveness of convergence of the ANN and theoretical approaches to experimental results were evaluated.

2. General characteristics of columns

2.1. Moment capacities of columns

Capacities of columns exposed to combine bending (N + M) are determined by writing equations of compliance amounting reinforcement sequence and two equations of equilibrium. A typical circular column section exposed to axial load N and strain diagram is shown in Fig. 1. Moment capacity of this element M_r , is calculated by the generalized formula in Eq. (1), after the height of the compression area, c, is identified. Strength recovery that occurs in the concrete core is ignored in this formulation. Even though it is possible to derive equations to determine the capacity of columns, using these equations for each and every N or M is rather troublesome. Therefore, calculations of load-bearing capacity of columns are made more easily via design tables and computer programs. Strength values given in Eqs. (1) and (2) should be considered as characteristic values for design and current (measured) strength for verification.

$$M_r = N_r \times e = 0.85f_c A_{cc} (x_p - \bar{x}) + \sum_{i=1}^n A_{si} \sigma_{si} x_i \tag{1}$$

$$N_r = 0.85f_c A_{cc} + \sum_{i=1}^n A_{si} \sigma_{si} \tag{2}$$

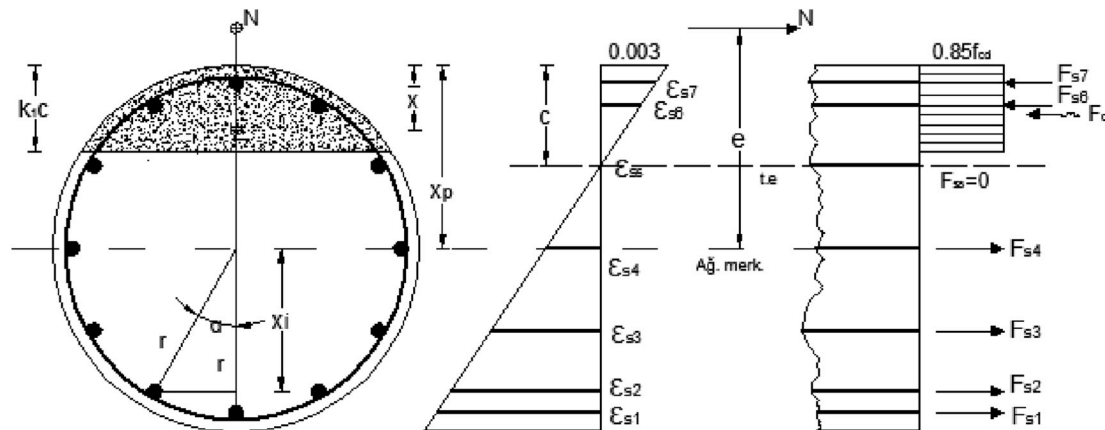


Fig. 1. Circular column under combined bending.

2.2. Shear force capacities of columns

Analytic formulas to calculate the shear strength of circular columns are present in many reinforced concrete building regulations such as the American Concrete Institute (ACI 318-08) [9], Design of Concrete Structures (CSA) [11], The Shear Strength of Reinforced Concrete Members (ASCE-ACI) [12], Specification for Design and Construction of Concrete Structure (JSCE) [13], Reinforced Concrete Structures Design and Construction Rules (TBC 500-2000) [14], and shear strength of circular columns in the empirical expressions contained in these regulations is calculated by taking the contribution of concrete and confinement reinforcement. Therefore, it is accepted that a portion of the design shear force is carried by concrete (V_c) and the remaining portion is carried by transverse reinforcement (V_s).

$$V_r = V_s + V_c \quad (3)$$

The equation below is given in ACI 318-08 [9] earthquake regulation in order to calculate the contribution of concrete (V_c) to the shear strength of elements exposed to shear, bending, and axial pressure [9].

$$V_c = 0.166 \left(1 + \frac{P}{13.80A_g} \right) \sqrt{f'_c} b d (\text{Units : MPa}) \quad (4)$$

Here, P is the axial load that the column is exposed to; A_g is a gross cross-sectional area of the column; f'_c is the compressive strength of the concrete; b is column width, and d is the effective depth of the column. The contribution of transverse reinforcement, V_s :

$$V_s = \frac{A_v f_y d}{s} \quad (5)$$

is calculated with Eq. (5). Here, A_v is transverse reinforcement area, f_y is yield strength of circular stirrup or spiral reinforcement and s is the spacing of transverse reinforcement.

According to TBC 500-2000 [14], the contribution of concrete to shear strength V_c is calculated by taking 80% of the cracking strength (V_{cr}) of the reinforced concrete section at shearing [10]. Cracking strength of concrete at shearing (diagonal cracking strength), V_{cr} is calculated with the following equation:

$$V_{cr} = 0.65 \times f_{ct} \times b_w \times d \times \left(1 + \gamma \frac{N_d}{A_c} \right) \quad (6)$$

$$V_c = 0.80 V_{cr} \quad (7)$$

Here, N_d is the design axial load of the column; A_c is the cross-sectional area of the column; f_{ct} is the tensile strength of the concrete; b_w is the column width; d is the effective depth of the column and γ is the coefficient reflecting impact of the axial load on the cracking strength (in case of axial pressure, $\gamma = 0.07$ in case of axial tension, $\gamma = -0.3$). The contribution of transverse reinforcement, V_s is calculated

with Eq. (8):

$$V_s = \left(\frac{A_{sw}}{s} \right) f_{yw} d \quad (8)$$

Here, A_{sw} is the sum of cross-section areas of confinement reinforcement, s is the confinement reinforcement spacing, f_{yw} is the yield strength of confinement reinforcement, and d is the effective depth of column.

2.3. Displacement ductility

Ductility is the plastic deformation ability of structure and constituting elements without any significant loss of strength and rigidity [15]. Among the ductility parameters, displacement is the most appropriate to evaluate the behavior of the structure and columns. The ductility of a cantilever column is determined by the ratio of ultimate displacement to yield displacement.

When calculating displacement ductility, various alternative methods have been offered to identify yield and ultimate displacement on the load-displacement curve as a result of experimental studies conducted by various researchers [15–17]. In this study, yield displacement is obtained by idealizing load-displacement envelope curve according to the two-line elasto-plastic behavior model (Fig. 2). In addition, ultimate displacement is determined by taking into account a certain amount of strength loss following the maximum load.

3. Artificial intelligence

The Artificial Neural Network (ANN) has been widely used to forecast difficult engineering problems. In the literature, the comparison between the ANN and other nonlinear regression model using error analysis showed that the ANN has good forecasting value for estimation capacity. Also in the literature it is well known that the percentage of error analysis using Mean Absolute Percentage Error (MAPE) for ANN produced less error than the linear and nonlinear regression. On the other hand, it is still discussed that some combined ANN and new generation soft computing methods can give a better results than conventional ANN.

3.1. Artificial neural networks (ANNs)

ANN might be considered as a logically programmed mechanism which was developed with the inspiration from the biological nervous system and which aims to generate the basic operations of the human brain with a certain software. A basic ANN cell in engineering has a simpler structure than a biological nerve cell and is defined as a processing element which connects the data obtained from the external environment to neurons via weights and produces an output by

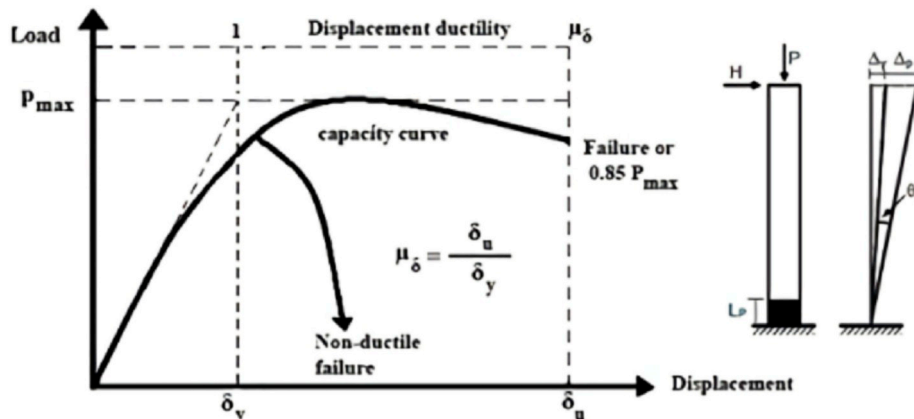


Fig. 2. Determination of yield and ultimate displacements of columns.

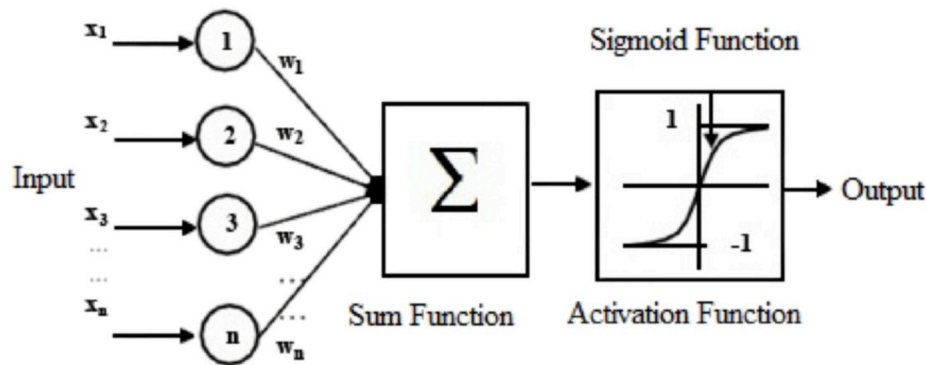


Fig. 3. A basic ANN cell [7].

determining the impact of these weights on the input when the sum of inputs exceeds the internal threshold value. The weights here are updated for all new data and the connection to neuron means the result of the multiplication of inputs with weights corresponding to these inputs with the help of sum function [18]. The result obtained passes through the activation function, calculates the net output during the operation and also generates the neuron output of this operation. The activation function is generally a non-linear function. A mathematical model of a simple neuron cell is shown in Fig. 3.

4. Composing a data set and selection of parameters

In this section, moment and shear force capacities and ductility values of spiral columns having different features are attempted to be estimated with four different ANNs. The dataset is obtained from the data bank comprising tests conducted by different researchers at the Pacific Earthquake Engineering Research Center (PEER) and in the literature. The experimental features of 79 spiral column test elements in this set, such as column section and height, mechanical features and ratios of longitudinal and transverse reinforcement, mechanical feature of concrete, axial load ratio and concrete cover, are taken into consideration to obtain moment and load-bearing capacities of columns, and continuity value of displacement ductility obtained via displacement sizes between yield and ultimate strength are arranged as shown in APPENDIX-1. Randomly selected 50 test elements among 79 test elements constituted the training set of the ANN algorithm while 29 test elements formed the test group. The test data are stated in terms of intended use (training or test) in the table in APPENDIX-1. It is observed in the experiments that columns are generally broken under the impact of bending or flexure + shear (shear flexural) and only a few reached its capacity due to shearing. In the study, a verification set involving 7 spiral columns compiled from literature was formed and it was tested.

In order for the accuracy of the study, it is crucial to determine ANN

architecture that will be used to determine moment and shear force capacities of reinforced concrete spiral columns under vertical and horizontal loads and their displacement ductility and to obtain the results within the optimum period. Therefore, 9 parameters to represent the input layer of the training algorithm, variables of problem and value of a column in the output layer are specified. These nine parameters are the parameters found in the empirical formulas used to calculate the moment and shear force carrying capacities of the reinforced concrete columns. In order to minimize the selection of input data in this layer and to ensure homogeneity of inter-column values, input parameters are composed by using processes such as column diameter and concrete cover instead of column area, axial load ratio instead of axial load, and longitudinal and transverse ratios instead of reinforcements. Since the column diameter D and length L are selected as parameters in the input layer, the slenderness ratio that are related to H/L are not considered as a parameter. Input parameters and numerical change ranges of training and test set are shown in Table 1.

The number of processing elements in the output layer is formed by the definition of the problem. Four different network architectures are created in this study. These network architectures are named ANN₁, ANN₂, ANN₃, and ANN₄. Model ANN₁ has three neurons in output layer and moment and shear force capacities of spiral columns and their ductility are estimated simultaneously. ANN₂, ANN₃, and ANN₄ network architectures have one output neuron; moment capacity, shear force capacity and section ductility are estimated respectively. The input layers of the four network structures are the same. However, while the output layer of the ANN₁ model has three neurons, the ANN₂, ANN₃ and ANN₄ network architectures have a single output neuron. The outputs in the ANN₁ model cover the outputs of the other three ANN's. Moment and shear force capacities of spiral columns are obtained from the test results. Ductility capacities are also calculated by load-displacement graphics obtained from the tests. For example, how the yield and failure displacement values calculated based on horizontal load (shear force) that cantilever column would bear by using

Table 1
Input parameters and change ranges of training and test set.

| No | Symbol | Input Parameters | Minimum Value | Maximum Value |
|----|----------|--|---------------|---------------|
| 1 | D | Diameter (mm) | 152 | 1520 |
| 2 | d' | Concrete cover (mm) | 9,7 | 60,3 |
| 3 | L | Column effective length (mm) | 570 | 9140 |
| 4 | f_c | Concrete compressive strength (MPa) | 23,1 | 90 |
| 5 | f_y | Yield strength of longitudinal reinforcement (MPa) | 296 | 507,5 |
| 6 | ρ_t | Longitudinal reinforcement ratio (%) | 0,52 | 5,57 |
| 7 | f_{yw} | Yield strength of transverse reinforcement (MPa) | 300 | 1000 |
| 8 | ρ_s | Volumetric reinforcement ratio (%) | 0,13 | 3,43 |
| 9 | N/N_o | Axial load ratio (%) | 0,08 | 0,42 |

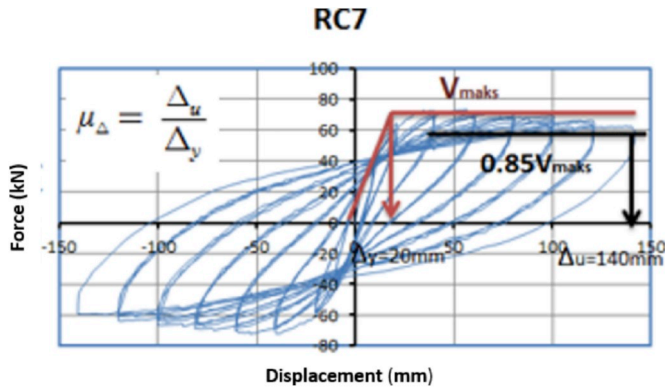


Fig. 4. Saatcioglu and Baingo (1999) lateral load-displacement curve belonging to RC7 test element [19].

Table 2
Output parameters and change ranges of training and test set.

| No | Symbol | Output Parameters | Minimum Value (kN-m) | Maximum Value (kN-m) |
|----|--------|-------------------|----------------------|----------------------|
| 1 | M | Moment | 22 | 14500 |
| 2 | V | Shear | 14 | 2968 |
| 3 | μ | Ductility | 1,23 | 14,04 |

load-displacement graph obtained from Saatcioglu and Binguo [20], RC7 test is shown in Fig. 4.

Input parameters and numerical change ranges of training and test set are shown in Table 2.

The input and output data in ANN are subjected to normalization process to provide homogeneity between columns before getting trained in the network. There are numerous data normalization techniques in the literature. Some of them are Median, Rule of Minimum, Rule of Maximum, Sigmoid, and Z-Score [20]. The data set used in this study is subjected to a scaling procedure between [0, 1]. In order to achieve this, min-max normalization technique is preferred as in studies of Pu [21], Arslan [3], and Koroglu [22], and scaling is made by using the formula given in Eq. (9) The values of training and test data after normalization procedure are given in the table in APPENDIX-2.

$$x' = \frac{x_i - x_{\min}}{x_{\max} - x_{\min}} \tag{9}$$

In Eq. (9) x' is the normalized value of x_i input value and, x_{\max} and x_{\min} respectively represent the highest and lowest values in the input set.

There are numerous criteria values in the literature which are used to evaluate the accuracy of estimation of established ANN models. The simplest error term among these values is calculated by means of finding the error value between real values and estimated values ($y(t) = T_{\text{real}} - T_{\text{estimate}}$) [23]. In this study, the most commonly used performance criteria values in literature shown in Table 3 are examined [24–26].

Here, P is the number of test data, o_i is the estimated value, t_i is the target value, m is the number of test data and n is the number of elements in the output layer of ANN. The accuracy of classification is obtained from Eq. (10) [27].

$$\text{Classification accuracy (\%)} = 100 - \text{Test Error} \tag{10}$$

Table 3
Performance criteria values.

| |
|--|
| The coefficient of determination (R^2), $R^2 = 1 - \left(\frac{SS_{\text{err}}}{SS_{\text{tot}}} \right)$, $R^2 = 1 - \left(\frac{\sum_{i=1}^P (t_i - o_i)^2}{\sum_{i=1}^P t_i^2 - \frac{(\sum_{i=1}^P t_i)^2}{P}} \right)$ |
| Root Mean Square Error (RMSE), $RMSE = \sqrt{\frac{\sum_{i=1}^P (t_i - o_i)^2}{P}}$ |
| Mean Absolute Error (MAE), $MAE = \frac{1}{P} \sum_{i=1}^P t_i - o_i $ |
| Mean Absolute Percentage Error (MAPE), $MAPE = \frac{1}{P} \sum_{i=1}^P \frac{ t_i - o_i }{o_i} \times 100$ |
| Test Error (TE), $\text{Test Error (\%)} = \left(\frac{\sum_{i=1}^P t_i - o_i }{m \times n} \right) \times 100$ |

Table 4
Training algorithms used in ANN.

| | |
|-----|---|
| BFG | Broyden- Fletcher- Goldfarb-Shanno |
| BR | Bayesian Regularization |
| CGB | Conjugate Gradient with Powell/Beale Restarts |
| CGF | Fletcher-Powell Conjugate Gradient |
| CGP | Polak-Ribiere Conjugate Gradient |
| GD | Gradient Descent |
| GDM | Gradient Descent with Momentum |
| GDA | Variable Learning Rate Gradient Descent |
| GDX | Gradient Descent with Adaptive Learning |
| LM | Levenberg-Marquardt |
| OSS | One Step Secant |
| SCG | Scaled Conjugate Gradient |

5. ANN training and results

The number of hidden layers of ANN model and the number of processing elements in the hidden layer is determined by means of the trial-and-error method as in similar studies [1–28]. During trial-and-error method learning, momentum and iteration values are fixed and firstly, numbers of hidden layers and processing elements of hidden layers are determined. By raising the number of hidden layers of ANN models incrementally from 1 to 3 and the number of neurons in the hidden layer from 2 to 50, numbers of optimum hidden nodes and hidden nodes cells are obtained in values where the training and test errors are the lowest. When performing these operations, the values of momentum, learning coefficient and iteration are kept fixed. Later on, the number of iterations is changed and the network architecture with the lowest training and test error is established. Performances of ANN models are evaluated with R^2 (determination coefficient). Feed-forward networks are the most commonly used network model in ANN and since they do not have a loop within themselves, they produce output data quickly without any delay. The feed-forward neural network has drawn great interest in many applications due to its universal approximation capability [29]. In this study 12 different feed-forward back propagation algorithms were used. These feed-forward back-propagation algorithms which can update weight and bias values of network parameters and back-propagate the error are used to train ANN models created in MATLAB program (Table 4).

The quadratic mean of error between the expected value and the estimated value (MSE) is used as a performance function during the training of the ANN model; a sigmoid function which can address wide input range in hidden layers and provide a smooth transition between values is used as a transfer function and purelin function is used in the output layer. Delta rule which adapts itself by intending to minimize quadratic mean of error between expected output and output produced by the network is used as adaptive learning function. Training

Table 5
Optimum ANN parameters.

| ANN Models | Target | Number of H.L. ^a | H.L. ^a Number of Nodes | Number of Iterations | Learning Duration (sec) | Learning Ratio | Momentum Coefficient |
|------------------|-----------------------------------|-----------------------------|--------------------------------------|----------------------|-------------------------|----------------|----------------------|
| ANN ₁ | M _r -V _r -μ | 2 | 17-5 | 100000 | 288 | 10 | 0,01 |
| ANN ₂ | M _r | 1 | 3 | 5000 | 10 | 10 | 0,01 |
| ANN ₃ | V _r | 2 | 13-3 | 38000 | 70 | 10 | 0,01 |
| ANN ₄ | μ | 3 | 13-3-17 | 5000 | 15 | 10 | 0,01 |

^a H.L.=Hidden Layer.

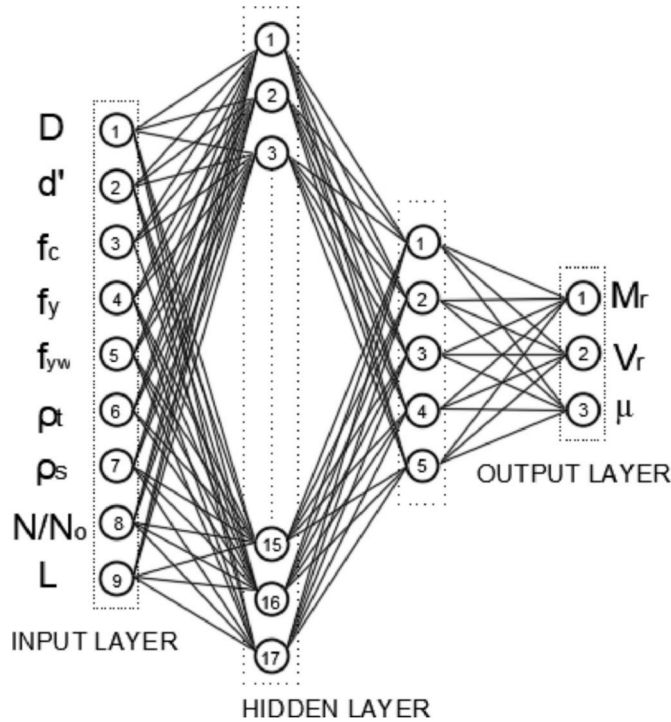


Fig. 5. Network architecture of ANN₁ model.

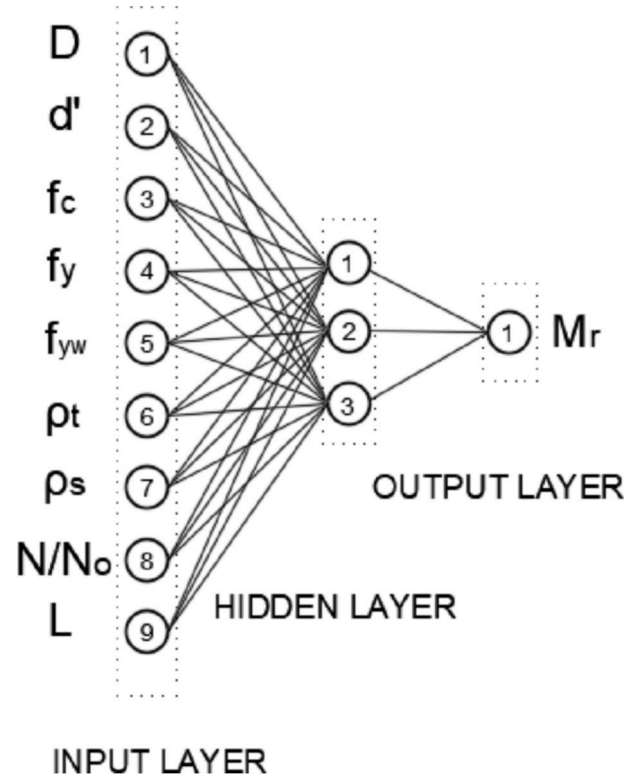


Fig. 6. Network architecture of ANN₂ model.

parameters belonging to ANN models are shown in Table 5 and network structures are shown in Figs. 5–8.

At the end of training, the values of moment, shear and ductility are normalized. To compare these values with actual values, conversion is applied with a correlation of Eq. (11).

$$x_i = x' \times (x_{max} - x_{min}) + x_{min} \quad (11)$$

5.1. Results of ANN₁ model

R², RMSE, MAE, MAPE, Test Error results used to evaluate performances of ANN models are shown in Table 6 for ANN₁ model. According to the results, for ANN₁ model's 12 different training algorithms, R² values were obtained between 0.9499 and 0.16. It is determined that the network model created with the SCG algorithm which has the highest R² value and the lowest RMSE, MAE, MAPE and Test Error values is the most appropriate model among the models created to obtain a moment, shear and section ductility capacities of spiral columns. The resulting value of 94.99% R² value of sensitivity analysis shows that 94.99% of the total change is determined by the established model, that is, by independent or dependent variables, 5.01% occurs accidentally or by other disregarded variables. The data obtained by the test results of moment, shear and ductility capacities of spiral columns are compared with the estimation results obtained from ANN₁ model in Fig. 9 and it is observed that ANN₁ is successful with a sufficient sensitivity ratio of 94.99%.

The impacts of output parameters on network performance of ANN₁ model are separately shown in Fig. 10. As seen from distribution diagrams moment capacity was R² = 96.49%, shear force capacity was R² = 87.34%, section ductility capacity was R² = 75.05%. It is normal that the estimated values of ANN's moment capacity were more convenient than the estimated value of shear force capacity since no classification is made in terms of failure type of columns when test data set is organized and damage is caused by bending in most of the columns during tests. It is observed that the ductility value could not reach the convergence level of the other two output parameters.

5.2. ANN₂ model results

Performance criteria values for ANN₂ model are shown in Table 7. According to the results, for 12 different training algorithms of ANN₂ model, R² values change between 0.5033 and 0.9762. It is determined that the network model created with the SCG algorithm which has the highest R² value and the lowest RMSE, MAE, MAPE and Test Error values is the most appropriate model among the models created to obtain a moment, shear and section ductility capacities of spiral columns. Sensitivity analysis result shows that ANN₂ model is quite successful in estimating moment capacity with R² sensitivity ratio of 97.62%. Fig. 11 shows the distribution diagram of monitored and predicted values of the SCG algorithm while Fig. 12 shows a graphical presentation of the estimated values and actual values.

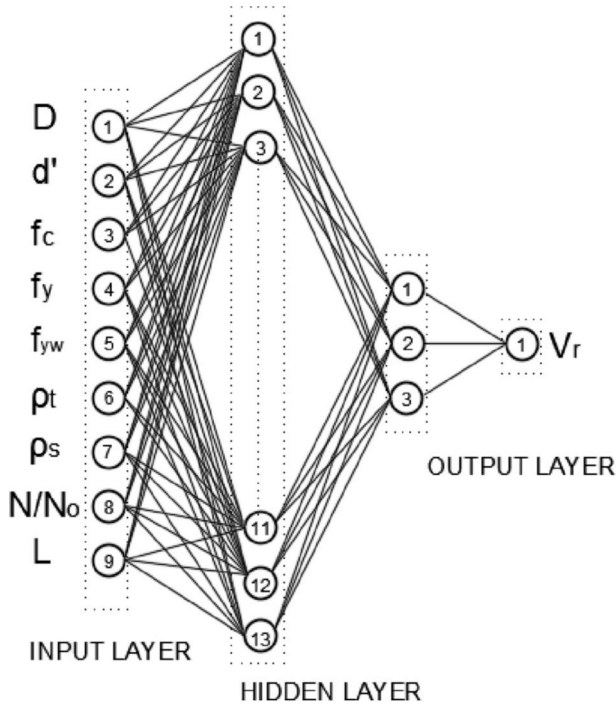


Fig. 7. Network architecture of ANN₃ model.

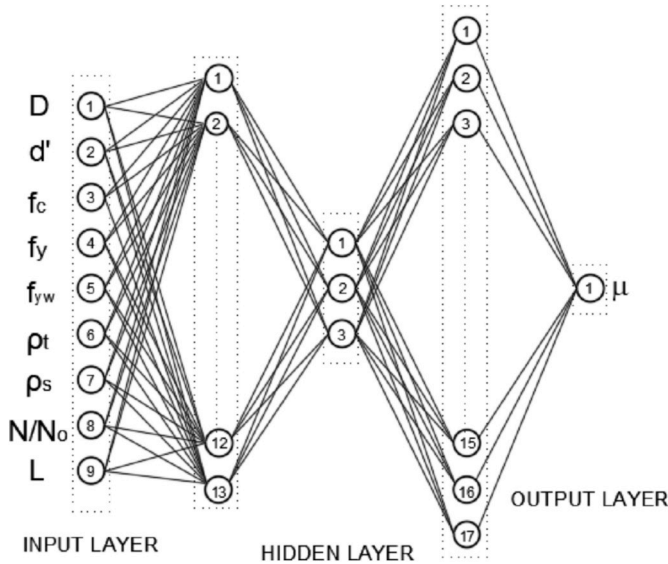


Fig. 8. Network architecture of ANN₄ model.

5.3. ANN₃ model results

Criteria parameters such as R², RMSE, MAE, MAPE, Test Error used to evaluate performances of ANN models are shown in Table 8 for ANN₃

Table 6
Criteria results of ANN₁ model obtained by analysis.

| ANN training algorithms | | BFG | BR | CGB | CGF | CGP | GD | GDM | GDA | GDX | LM | OSS | SCG |
|-----------------------------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|
| Results of ANN ₁ Model | R ² | 0,56 | 0,62 | 0,76 | 0,7355 | 0,8339 | 0,8232 | 0,8235 | 0,9076 | 0,8393 | 0,1664 | 0,4804 | 0,9499 |
| | RMSE | 0,1634 | 0,1646 | 0,1279 | 0,1316 | 0,0971 | 0,1109 | 0,1139 | 0,081 | 0,0971 | 0,3967 | 0,2789 | 0,0776 |
| | Test Error | 6,8755 | 6,1362 | 6,0782 | 5,2706 | 4,5147 | 6,7409 | 6,735 | 4,7145 | 4,8004 | 12,357 | 8,4137 | 4,0562 |
| | MAE | 0,0688 | 0,0614 | 0,0608 | 0,0527 | 0,0451 | 0,0674 | 0,0673 | 0,0471 | 0,048 | 0,1236 | 0,0841 | 0,0406 |
| | MAPE | 0,4448 | 0,397 | 0,3932 | 0,341 | 0,2921 | 0,4361 | 0,4357 | 0,305 | 0,3106 | 0,7995 | 0,5443 | 0,2624 |

model. According to the results, for 12 different training algorithms of ANN₃ model, R² values change between 0.2336 and 0.9621. It is determined that the network model created with the SCG algorithm which has the highest R² value and the lowest RMSE, MAE, MAPE and Test Error values is the most appropriate model among the models created to obtain shear capacities of spiral columns. Sensitivity analysis result shows that ANN₃ model is quite successful in estimating shear force capacity with R² sensitivity ratio of 96.21%. Fig. 13 shows the distribution diagram of the observed and predicted values of the SCG algorithm while Fig. 14 shows a graphical presentation of the estimated values and actual values.

5.4. ANN₄ model results

Performance criteria parameters such as R², RMSE, MAE, MAPE, and Test Error are shown in Table 9 for ANN₄ model. According to the results, R² values for 12 different training algorithms of ANN₄ model changes between 0.2338 and 0.7760. It is determined that the network model created with the SCG algorithm which has the highest R² value and the lowest RMSE, MAE, MAPE and Test Error values is the most appropriate model among the models created to obtain section ductility capacities of spiral columns.

Sensitivity analysis result shows that ANN₄ model is not quite successful in estimating section ductility with R² sensitivity ratio of 77.60%. Fig. 15 shows the distribution diagram of the observed and predicted values of the SCG algorithm while Fig. 16 shows a graphical presentation of the estimated values and actual values.

6. Verification set

In this section of the study, a verification set involving 7 spiral columns used as test elements which are compiled from literature independent of test and training set is formed to measure the performance accuracy of ANN₁ network model (Table 10). The verification set shown in Table 10 is tested with the network model ANN₁ which has the most complex structure proposed and the moment and shear force capacities along with ductility values of circular spiral columns are estimated. The estimation results of verification set show that the estimation result values of ANN1 model and test results are rather close to each other and the proposed model is successful with a classification accuracy of 80.78% (Table 11).

As a result of the sensitivity analysis, R² values for the moment, shear and ductility parameters and convergence successes were obtained with 88.87%, 98.75%, and 16.69% precision respectively. It is seen that the success of predicting moment and shear force capacities of spiral columns in network model ANN₁ is better than the success of predicting displacement ductility. The main reason for this is considered to be the fact that the displacement ductility values are rather low in comparison to the values of moment and shear. Fig. 17 shows the distribution diagram of observed and predicted values of verification set.

The shear force capacities of spiral column test elements included in the verification set are compared with the theoretical approaches specified in reinforced concrete construction regulations [9,14] in Table 12. When the contribution of concrete is calculated in the

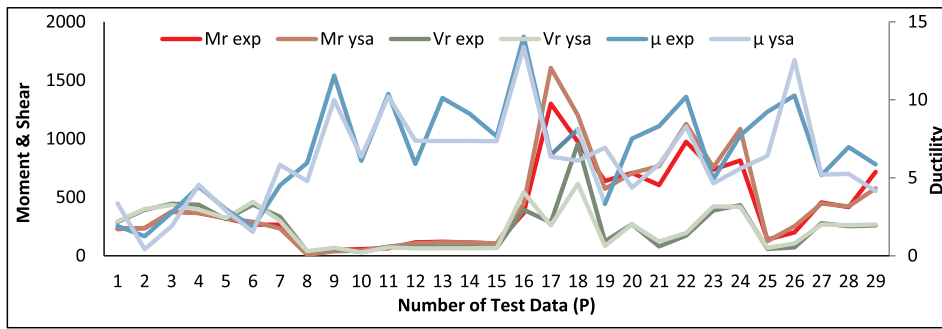


Fig. 9. Graphic presentation of estimated values and actual values of SCG training function of ANN₁ model.

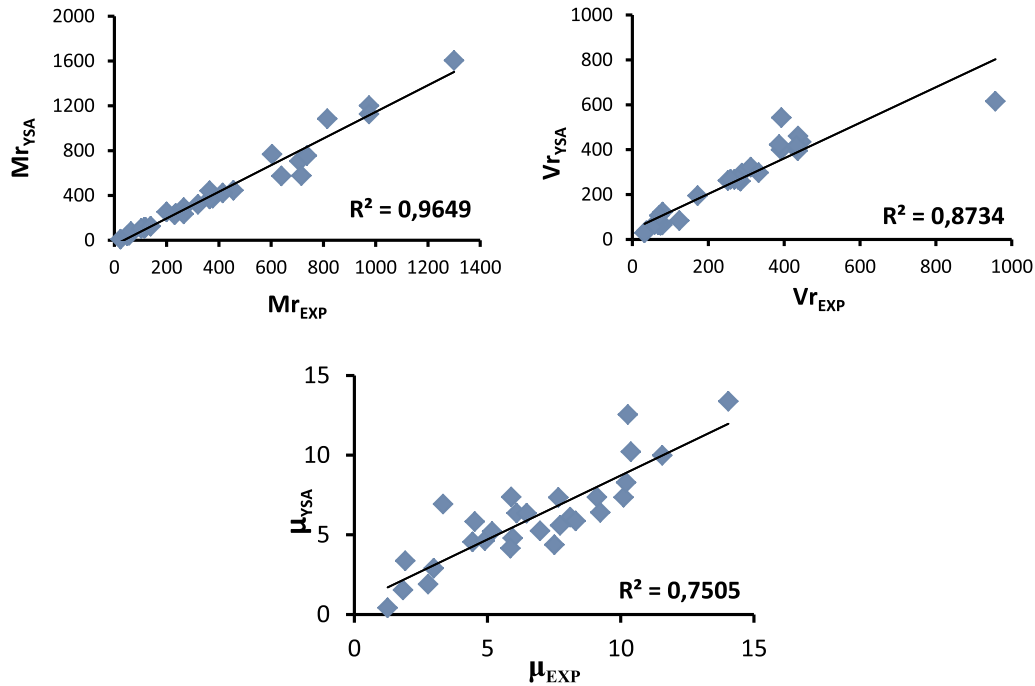


Fig. 10. Comparison of the estimated moment, shearing and ductility values of ANN₁ model with test results.

Table 7

Criteria results of ANN₂ model obtained by analysis.

| ANN training algorithms | | BFG | BR | CGB | CGF | CGP | GD | GDM | GDA | GDX | LM | OSS | SCG |
|-------------------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|
| Results of ANN2 Model | R ² | 0,9585 | 0,9295 | 0,5033 | 0,7449 | 0,8465 | 0,7355 | 0,6706 | 0,8494 | 0,8469 | 0,9576 | 0,8091 | 0,9762 |
| | RMSE | 0,0046 | 0,0071 | 0,0163 | 0,013 | 0,0089 | 0,0132 | 0,0199 | 0,0088 | 0,009 | 0,0047 | 0,0099 | 0,0035 |
| | Test Error | 0,301 | 0,3765 | 1,1232 | 1,0191 | 0,6544 | 0,9261 | 1,3473 | 0,7283 | 0,5523 | 0,2762 | 0,5685 | 0,2268 |
| | MAE | 0,003 | 0,0038 | 0,0112 | 0,0102 | 0,0065 | 0,0093 | 0,0135 | 0,0073 | 0,0055 | 0,0028 | 0,0057 | 0,0023 |
| | MAPE | 0,3922 | 0,4905 | 1,4633 | 1,3276 | 0,8525 | 1,2066 | 1,7552 | 0,9489 | 0,7195 | 0,3598 | 0,7406 | 0,2954 |

calculation of shear force capacity, axial load levels on columns are also taken into consideration. The types of failure occurred in columns when the column reaches load-bearing capacity during tests are specified in tables for each test element. Among the test elements, only the test element no. 2 reached failure state due to shear capacity and the experimental shear force capacity value of this column is obtained with a ratio of 1.072 to the closest result by TBC 500-2000 regulation. But when the mean of shear force capacity rates of all test elements are taken into consideration, the worst result is obtained from TBC 500-2000 with the rate of 0.55 and a rather successful result is obtained with the rate of 1.002 with the recommended ANN₁ model. The calculated shear force capacities of test elements 3/4/5/7 in accordance

with theoretical approaches stated in reinforced concrete construction regulations and their experimental shear force capacity values are quite different as shown in Table 12. The reason for this difference is that these test elements reach their horizontal load bearing capacities due to bending before they reach their shear force capacities calculated in accordance with theoretical approaches. Fig. 18 shows the load-displacement curves of sample columns which reach their horizontal load bearing capacities due to bending and shear force. As shown in these curves, there is no increase of horizontal load in the ductile section due to bending and it continues to bear the load by increasing displacement under a fixed horizontal strength.

A comparison is made between experimental moment capacities of

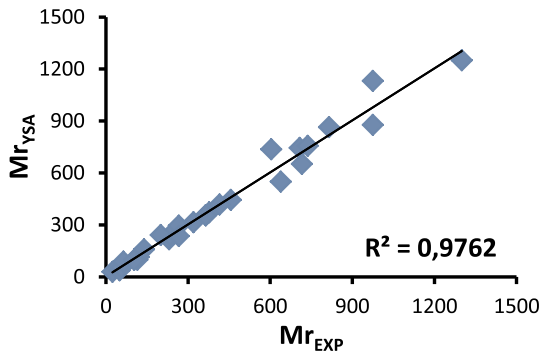


Fig. 11. Moment distribution diagram of the SCG training algorithm of ANN₂ model.

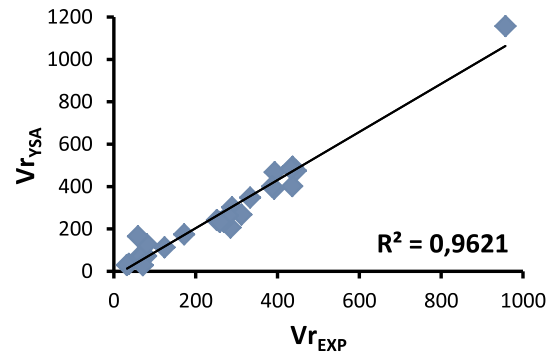


Fig. 13. Distribution diagram of shear values SCG training algorithm of ANN₃ model.

spiral column test elements included in the verification set and theoretical approaches specified in the reinforced concrete construction regulations in Table 13. As a result of this comparison, among the ratio means of experimental moment capacities of spiral columns in the verification set and the ratio means of moment capacities obtained by using equations in regulations: the worst result is obtained with ACI 318-08 regulation as 1.29 and the closest result is obtained in the recommended ANN model with TBC 500-2000 with the rate of 0.9942 and rate of 1.13, respectively. It is seen in the light of results that the network model created in this study provides more appropriate results which are fairly close to the actual data than the reinforced concrete regulations.

7. Conclusions

In this study, an ANN based algorithm is developed to estimate the moment and shear force capacities and the displacement ductility of a reinforced concrete spiral column by means of the data obtained from 86 spiral column tests carried out experimentally in literature. It is found in the study that the moment and shear force capacities and the displacement ductility of spiral columns are more precisely estimated in comparison to the empirical approaches specified in the reinforced concrete regulations. The Network performance of the recommended

and developed ANN network model has tested again by means of the verification set which is particularly independent of the selected data set and it is observed that the ANN model would be reliably used due to its success to estimate the moment and shear force capacities and the displacement ductility of spiral columns simultaneously.

The moment and shear force capacities and the displacement ductility of the network structures named ANN₁, ANN₂, ANN₃, ANN₄ led to encouraging results of 94.49%, 97.62%, 96.21%, 77.60% respectively and this proved that ANN has a potential use in this field. In addition, the success of the verification set shows that it could be used as an alternative method to overcome the difficulties in estimating the moment and shear force capacities and displacement ductility of a spiral column.

It is seen that the SCG algorithm is more successful than other feed-forward back-propagation training algorithms. The closest result to the SCG algorithm is obtained with the GDA algorithm as 90.76% in network architecture named ANN₁.

The results of ANN₁ and ANN₄ showed that they are far off the estimation results of the moment and shear force capacities in predicting displacement ductility of spiral columns. It is considered that the main reason for this finding is the acceptances made in the determination of displacement values in yield and collapse positions. Moreover, as the ductility values are numerically lower than the values

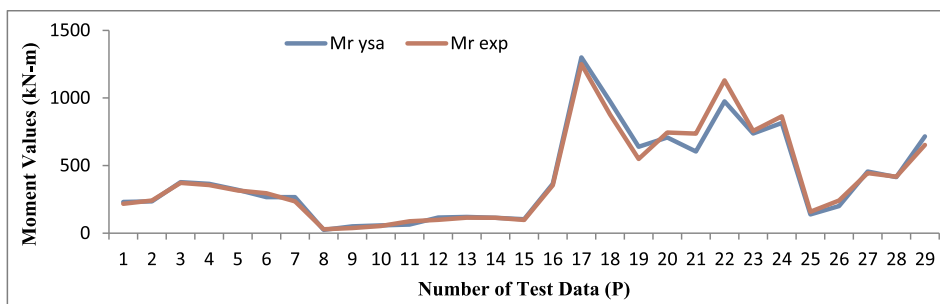


Fig. 12. Graphic presentation of estimated values and actual values of SCG training function of ANN₂ model.

Table 8
Criteria results of ANN₃ model obtained by analysis.

| ANN training algorithms | | BFG | BR | CGB | CGF | CGP | GD | GDM | GDA | GDX | LM | OSS | SCG |
|-----------------------------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|
| Results of ANN ₃ Model | R ² | 0,2336 | 0,5614 | 0,7381 | 0,9403 | 0,9557 | 0,5603 | 0,545 | 0,504 | 0,4567 | 0,7011 | 0,8551 | 0,9621 |
| | RMSE | 0,0658 | 0,0505 | 0,035 | 0,0171 | 0,0143 | 0,0444 | 0,0452 | 0,0469 | 0,0492 | 0,0473 | 0,0285 | 0,0178 |
| | Test Error | 2,7932 | 2,0629 | 1,3454 | 1,0106 | 0,8838 | 3,4828 | 3,52 | 2,055 | 1,9289 | 2,5542 | 1,3489 | 1,0791 |
| | MAE | 0,0279 | 0,0206 | 0,0135 | 0,0101 | 0,0088 | 0,0348 | 0,0352 | 0,0205 | 0,0193 | 0,0255 | 0,0135 | 0,011 |
| | MAPE | 1,2208 | 0,9016 | 0,5884 | 0,4417 | 0,3863 | 1,5222 | 1,5384 | 0,8981 | 0,843 | 1,1163 | 0,5895 | 0,4795 |

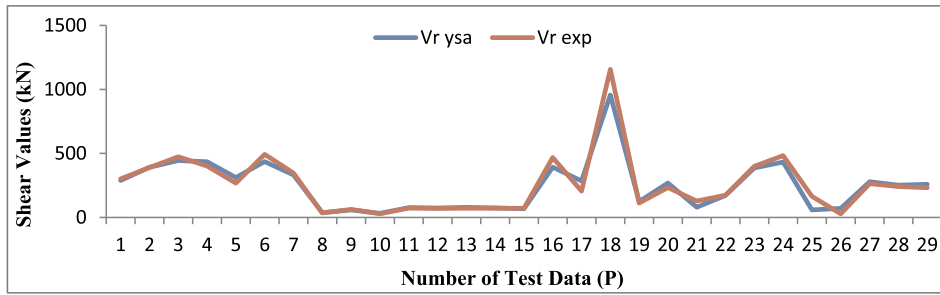


Fig. 14. Graphic presentation of estimated values and actual values of SCG training function of ANN₃ model.

Table 9

Criteria results of ANN₄ model obtained by analysis.

| ANN training algorithms | | BFG | BR | CGB | CGF | CGP | GD | GDM | GDA | GDX | LM | OSS | SCG |
|-----------------------------------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------|
| Results of ANN ₄ Model | R ² | 0,4302 | 0,6032 | 0,3551 | 0,2338 | 0,6467 | 0,3932 | 0,0811 | 0,4802 | 0,4739 | 0,5123 | 0,5688 | 0,776 |
| | RMSE | 0,2418 | 0,1822 | 0,274 | 0,2765 | 0,1591 | 0,2043 | 0,2521 | 0,1928 | 0,1911 | 0,1791 | 0,1649 | 0,1365 |
| | Test Error | 17,287 | 13,169 | 16,954 | 16,082 | 12,336 | 14,968 | 19,972 | 13,475 | 13,47 | 13,729 | 13,334 | 10,977 |
| | MAE | 0,1729 | 0,1317 | 0,1695 | 0,1608 | 0,1234 | 0,1497 | 0,1997 | 0,1348 | 0,1347 | 0,1373 | 0,1333 | 0,1098 |
| | MAPE | 1,394 | 1,0619 | 1,3672 | 1,2968 | 0,9947 | 1,207 | 1,6104 | 1,0866 | 1,0862 | 1,1071 | 1,0752 | 0,8851 |

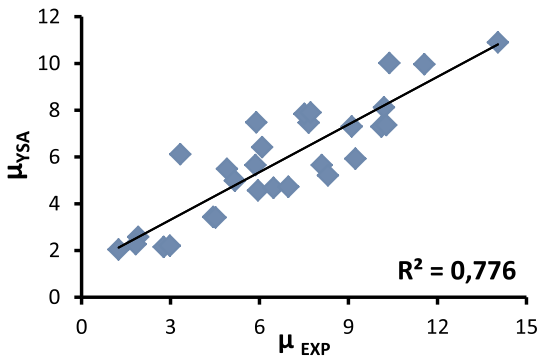


Fig. 15. Distribution diagram of ductility values of SCG training algorithm of ANN₄ model.

of moment and shear force values, it is assumed that the little differences between the predicted and estimated values increase the error percentage and consequently, increase the test error. On the other hand, when calculating displacement ductility, various alternative methods have been offered to identify yield and ultimate displacement on the load-displacement curve. In this study, yield displacement is obtained by idealizing load-displacement envelope curve according to the two-line elasto-plastic behavior model. Ductility capacity is not an

experimental result such as moment and shear force capacity and is determined according to the acceptances. Therefore, it varies according to the assumptions made. The effect of the input parameters was compared with IBM SPSS analysis program [30]. It is seen that the parameters effective in ductility capacity are effective in artificial neural networks. However, the estimation of the ductility capacity of artificial neural networks is not sufficiently successful. Therefore, it is considered that the effect on ductility capacity of approximate assumptions such as determination of yield displacement has a great effect, thus affecting the result to a great extent.

The effect of the nine parameters selected for the input layer on the parameters in the output layer was evaluated by correlation analysis using the IBM SPSS statistic program (Table 14). According to the results of correlation analysis, it was seen that column diameter D, cover thickness d' and column length L were effective for moment capacity (M_r). For the shear force capacity (V_r), the column diameter D, the cover thickness d, the volumetric ratio of the confinement reinforcement ρ_s along with the column length and the yield strength of reinforcement steel f_y were effective parameters. Also for the capacity of ductility (μ), the longitudinal reinforcement ratio ρ_t is determined as the most effective parameter. Other effective parameters for ductility are volumetric ratio of reinforcement ρ_s, yield strength f_y and also the axial load ratio N/N_o. In contrast to the reinforced concrete behavior, it is seen from the correlation distribution given in Table 14 that the concrete type (or concrete compressive strength f_c) and the yield strength

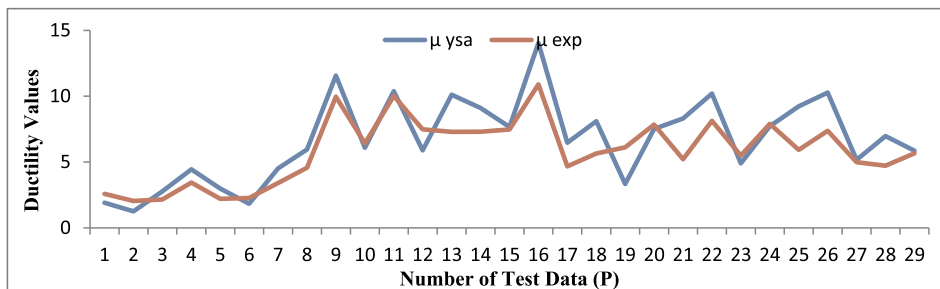


Fig. 16. Graphic presentation of estimated values and actual values of SCG training function of ANN₄ model.

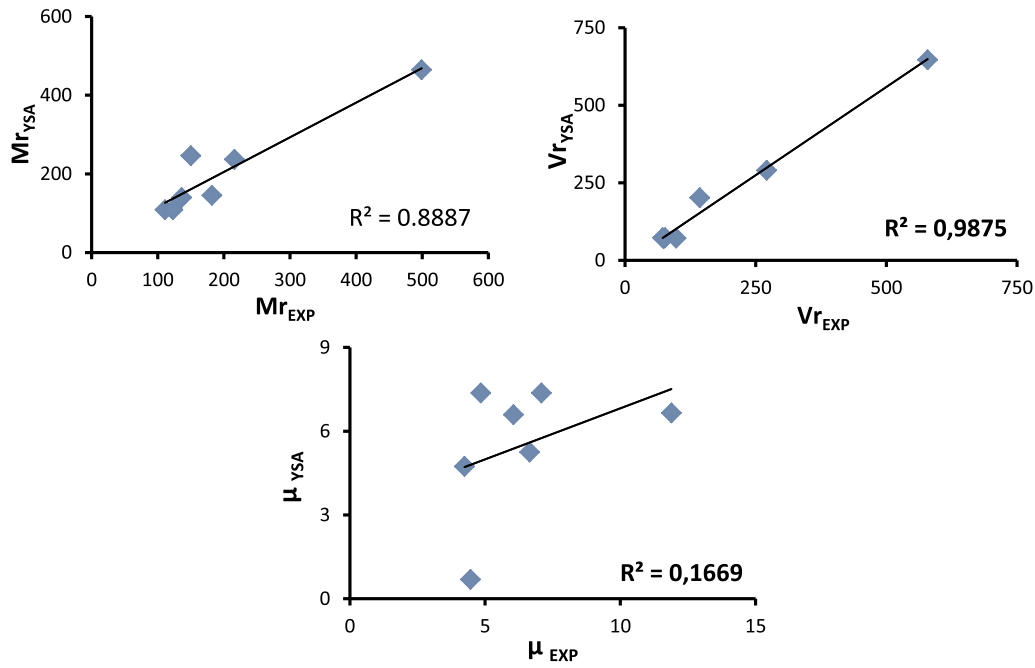


Fig. 17. Distribution diagram of verification set.

Table 10
Input parameter values of verification set.

| Specimen Name | D (mm) | d' (mm) | L (mm) | f _c (MPa) | f _y (MPa) | ρ _t (%) | f _{yw} (MPa) | ρ _s (%) | P _e /(f _c ² A _g) |
|--------------------------|--------|---------|--------|----------------------|----------------------|--------------------|-----------------------|--------------------|---|
| Wong et al., 1990, No. 3 | 400 | 20 | 800 | 37 | 475 | 3,2 | 300 | 1,42 | 0,39 |
| Ang et al., 1985, No. 21 | 400 | 18 | 800 | 33,2 | 436 | 3,2 | 326 | 0,38 | 0 |
| Kunnath et al., 1997, A4 | 305 | 14,5 | 1372 | 35,5 | 448 | 2,04 | 434 | 0,94 | 0,09 |
| Kunnath et al., 1997, A5 | 305 | 14,5 | 1372 | 35,5 | 448 | 2,04 | 434 | 0,94 | 0,09 |
| Hamilton, 2002, UC12 | 406,4 | 15 | 1854,2 | 36,5 | 458,5 | 1,17 | 691,5 | 0,53 | 0 |
| Hamilton, 2002, UC13 | 406,4 | 10,5 | 1047,7 | 34,7 | 458,5 | 1,37 | 691,5 | 0,1 | 0 |
| Hamilton, 2002, UC16 | 406,4 | 15 | 1854,2 | 35,6 | 458,5 | 1,17 | 691,5 | 0,53 | 0 |

Table 11
Comparison of test results of verification set with estimated results of ANN₁ model.

| Specimen Name | Experimental Result | | | ANN ₁ | | | Test Error (%) | | |
|--|---------------------|--------|-------|------------------|--------|------|----------------|---------------|---------------|
| | M (kN-m) | V (kN) | μ | M (kN-m) | V (kN) | μ | M | V | μ |
| Wong et al., 1990, No. 3 | 499 | 579 | 6,65 | 464,32 | 646,52 | 5,25 | 6,95 | 11,66 | 21,04 |
| Ang et al., 1985, No. 21 | 216 | 271 | 4,46 | 236,56 | 290,29 | 0,69 | 9,52 | 7,12 | 84,47 |
| Kunnath et al., 1997, A4 | 111 | 72 | 7,08 | 108,64 | 72,81 | 7,37 | 2,13 | 1,13 | 4,09 |
| Kunnath et al., 1997, A5 | 123 | 77 | 4,84 | 108,64 | 72,81 | 7,37 | 11,67 | 5,44 | 52,26 |
| Hamilton, 2002, UC12 | 136 | 74 | 6,05 | 139,49 | 69,73 | 6,59 | 2,57 | 5,77 | 8,92 |
| Hamilton, 2002, UC13 | 150 | 143 | 4,24 | 246,18 | 201,68 | 4,74 | 64,12 | 41,04 | 11,76 |
| Hamilton, 2002, UC16 | 182 | 98 | 11,89 | 145,38 | 71,45 | 6,65 | 20,12 | 27,09 | 44,05 |
| Mean Percentage Error | | | | | | | 16,724 | 14,177 | 32,369 |
| Test Error | | | | | | | 19,22 | | |
| Classification Accuracy (100-Test Error) | | | | | | | 80,78 | | |

of longitudinal reinforcement f_y are not effective in the ductility values along with the moment and shear force capacity. This can be explained by the fact that the reinforcement and concrete strength are not changed in a very wide range in the selected data set.

The moment and shear force capacities of test elements involved in the verification set are compared by means of experimental, ANN, and regulatory approaches. The results of the empirical formula contained in regulation are far from the results of the experimental and ANN

results. This is because the samples in the verification set reach to collapse mechanisms with different failure modes. When the result of the sample showing shear failure (failure type 2) is examined for the shear force capacity and the result of the samples having bending damage (failure type 1) for the moment capacity are examined, it is true that results of theoretical approaches might be evaluated more accurately. When the theoretical results are examined in this respect, it is seen that they are parallel to ANN and experimental results and ACI

Table 12
Comparison of shear force capacities of spiral columns included in verification set with traditional methods.

| No | Specimen Name | Failure Type | V_r (TS 500–2000) | V_r (ACI) | V_{ANN1} (ANN) | V_{EXP} (Experi-mental) | V_{EXP}/V_{TS} | V_{EXP}/V_{ACI} | V_{EXP}/V_{ANN1} |
|----------------|--------------------------|--------------|---------------------|-------------|------------------|---------------------------|------------------|-------------------|--------------------|
| 1 | Wong et al., 1990, No. 3 | 3 | 472,284 | 522,54 | 646,516 | 579 | 1,2259 | 1,10804 | 0,89556 |
| 2 | Ang et al. 1985, No. 21 | 2 | 252,623 | 195,26 | 290,290 | 271 | 1,0727 | 1,38789 | 0,93354 |
| 3 | Kunnath et al., 1997, A4 | 1 | 265,693 | 228,98 | 72,8130 | 72 | 0,2709 | 0,31443 | 0,98883 |
| 4 | Kunnath et al., 1997, A5 | 1 | 265,693 | 228,98 | 72,8130 | 77 | 0,2898 | 0,33627 | 1,05750 |
| 5 | Hamilton, 2002, UCI2 | 1 | 449,241 | 358,89 | 69,7267 | 74 | 0,1647 | 0,20619 | 1,06128 |
| 6 | Hamilton, 2002, UCI3 | 3 | 224,522 | 170,36 | 201,680 | 143 | 0,6369 | 0,83939 | 0,70904 |
| 7 | Hamilton, 2002, UCI6 | 1 | 447,030 | 357,35 | 71,4548 | 98 | 0,2192 | 0,27424 | 1,37149 |
| Average | | | | | | | 0,5543 | 0,63806 | 1,00246 |

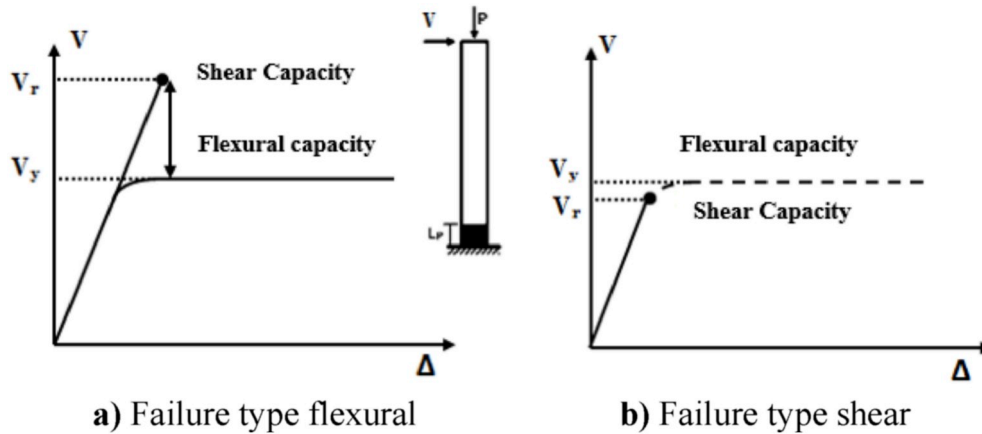


Fig. 18. Load-displacement curves of columns under horizontal load. a) Failure type flexural b) Failure type shear.

Table 13
Comparison of moment capacities of spiral columns included in verification set with traditional methods.

| No | Specimen Name | ^a Failure Type | M_r (TS 500–2000) | M_r (ACI) | M_{ANN1} (ANN ₁) | M_{EXP} (Experi-mental) | M_{EXP}/M_{TS} | M_{EXP}/M_{ACI} | M_{EXP}/M_{ANN1} |
|----------------|--------------------------|---------------------------|---------------------|-------------|--------------------------------|---------------------------|------------------|-------------------|--------------------|
| 1 | Wong et al., 1990, No. 3 | 3 | 348,5 | 313,84 | 464,32 | 499 | 1,43 | 1,59 | 1,07 |
| 2 | Ang et al., 1985, No. 21 | 2 | 250,2 | 240 | 236,56 | 216 | 0,86 | 0,90 | 0,91 |
| 3 | Kunnath et al., 1997, A4 | 1 | 98,8 | 91,74 | 108,64 | 111 | 1,12 | 1,21 | 1,02 |
| 4 | Kunnath et al., 1997, A5 | 1 | 98,8 | 91,79 | 108,64 | 123 | 1,24 | 1,34 | 1,13 |
| 5 | Hamilton, 2002, UCI2 | 1 | 134,6 | 113,33 | 139,49 | 136 | 1,01 | 1,20 | 0,97 |
| 6 | Hamilton, 2002, UCI3 | 3 | 159,1 | 131,58 | 246,18 | 150 | 0,94 | 1,14 | 0,61 |
| 7 | Hamilton, 2002, UCI6 | 1 | 138,8 | 112,35 | 145,38 | 182 | 1,31 | 1,62 | 1,25 |
| Average | | | | | | | 1,13 | 1,29 | 0,9942 |

^a Failure Type = 1: Flexure, 2: Shear, 3: Flexure-Shear.

Table 14
Correlation distribution of the values in the input layer on the parameters in the output layer.

| Correlations | D Diameter (mm) | d' Concrete cover (mm) | L (mm) | f _c (MPa) | f _y (MPa) | ρ _t (%) | f _{yw} (MPa) | ρ _s (%) | N/N _o |
|--------------|-------------------|---------------------------|-------------------|----------------------|----------------------|--------------------|-----------------------|--------------------|-------------------|
| Mmax (kN-m) | ,863 ^b | ,814 ^b | ,605 ^b | -,050 | ,192 | -,102 | -,008 | -,008 | ,032 |
| Vmax (kN) | ,774 ^b | ,760 ^b | ,237 ^a | -,146 | ,210 | ,013 | -,226 ^a | -,226 ^a | ,084 |
| μ | -,007 | -,079 | ,173 | ,001 | ,088 | ,348 ^b | ,296 ^b | ,296 ^b | ,298 ^b |

^a Correlation is significant at the 0.05 level (2-tailed).

^b Correlation is significant at the 0.01 level (2-tailed).

318-08 regulation is more reliable than TS 500–2000. No classification is made in terms of failure types of column samples when the current data set is prepared. It is assumed that having a sufficient number of data for each and every failure type in data set would lead to more appropriate results.

When the architecture of the network model is generated in the study, no tangible generalization is obtained with regard to the most appropriate number of hidden layers and of processing elements in hidden layers. Therefore, determination of the number of hidden layers and of the neurons in these layers is only possible with a trial-and-error

method for now. Even though the problems requested to be solved in the network are non-linear, appropriate results are obtained.

Increasing the number of test data used for training of network would facilitate learning and thus, more appropriate results might be

obtained. Because test data are used to verify, caliber or improve the ANN network models. Estimation of moment and shear force capacities and displacement ductility of ANN network model is dependent on the experimental test data set on which the model is based.

Appendix 1

Selected Data Set for Training and Testing

| No | Specimen Name | D (Diameter) (mm) | d' (Concrete cover) (mm) | L (mm) | fc (MPa) | fy (MPa) | ρ_l (%) | fyw (MPa) | ρ_s (%) | P _c / (f'c*Ag) | M _{max} (kN- m) | V _{max} (kN) | μ |
|----|-------------------------------|----------------------|-----------------------------|-----------|-------------|-------------|--------------|--------------|--------------|------------------------------|-----------------------------|--------------------------|-------|
| 1 | Ang et al., 1985, No. 1 | 400 | 18,00 | 800 | 37,5 | 436 | 3,20 | 328 | 0,51 | 0,00 | 256 | 321 | 1,81 |
| 2 | Ang et al., 1985, No. 2 | 400 | 18,00 | 800 | 37,2 | 296 | 3,20 | 328 | 0,51 | 0,00 | 175 | 219 | 5,79 |
| 3 | Ang et al., 1985, No. 4 | 400 | 20,00 | 800 | 30,6 | 436 | 3,20 | 316 | 0,51 | 0,00 | 231 | 289 | 1,91 |
| 4 | Ang et al., 1985, No. 5 | 400 | 18,00 | 800 | 31,1 | 436 | 3,20 | 328 | 0,76 | 0,00 | 265 | 331 | 1,55 |
| 5 | Ang et al., 1985, No. 6 | 400 | 18,00 | 600 | 30,1 | 436 | 3,20 | 328 | 0,51 | 0,00 | 235 | 392 | 1,25 |
| 6 | Ang et al., 1985, No. 7 | 400 | 18,00 | 800 | 29,5 | 448 | 3,20 | 372 | 0,38 | 0,00 | 225 | 281 | 1,23 |
| 7 | Ang et al., 1985, No. 8 | 400 | 18,00 | 800 | 28,7 | 448 | 3,20 | 372 | 1,02 | 0,20 | 377 | 445 | 2,77 |
| 8 | Ang et al., 1985, No. 9 | 400 | 18,00 | 1000 | 29,9 | 448 | 3,20 | 372 | 1,02 | 0,20 | 401 | 364 | 3,34 |
| 9 | Ang et al., 1985, No. 10 | 400 | 21,00 | 800 | 31,2 | 448 | 3,20 | 332 | 1,02 | 0,20 | 371 | 437 | 2,28 |
| 10 | Ang et al., 1985, No. 12 | 400 | 18,00 | 600 | 28,6 | 436 | 3,20 | 328 | 1,02 | 0,10 | 321 | 526 | 1,23 |
| 11 | Ang et al., 1985, No. 13 | 400 | 18,00 | 800 | 36,2 | 436 | 3,20 | 326 | 1,02 | 0,10 | 365 | 436 | 4,44 |
| 12 | Ang et al., 1985, No. 14 | 400 | 18,00 | 800 | 33,7 | 424 | 3,24 | 326 | 0,51 | 0,00 | 253 | 316 | 3,49 |
| 13 | Ang et al., 1985, No. 15 | 400 | 18,00 | 800 | 34,8 | 436 | 1,92 | 326 | 0,51 | 0,00 | 184 | 230 | 6,10 |
| 14 | Ang et al., 1985, No. 16 | 400 | 18,00 | 800 | 33,4 | 436 | 3,20 | 326 | 0,51 | 0,10 | 287 | 352 | 2,03 |
| 15 | Ang et al., 1985, No. 17 | 400 | 18,00 | 1000 | 34,3 | 436 | 3,20 | 326 | 0,51 | 0,10 | 320 | 312 | 2,98 |
| 16 | Ang et al., 1985, No. 18 | 400 | 18,00 | 600 | 35,0 | 436 | 3,20 | 326 | 0,51 | 0,10 | 309 | 505 | 2,29 |
| 17 | Ang et al., 1985, No. 19 | 400 | 18,00 | 600 | 34,4 | 436 | 3,20 | 326 | 0,38 | 0,10 | 266 | 437 | 1,83 |
| 18 | Ang et al., 1985, No. 22 | 400 | 20,00 | 800 | 30,9 | 436 | 3,20 | 310 | 0,39 | 0,00 | 228 | 285 | 2,91 |
| 19 | Ang et al., 1985, No. 23 | 400 | 21,00 | 800 | 32,3 | 436 | 3,20 | 332 | 0,76 | 0,00 | 266 | 333 | 4,52 |
| 20 | Ang et al., 1985, No. 24 | 400 | 20,00 | 800 | 33,1 | 436 | 3,20 | 310 | 0,77 | 0,00 | 272 | 341 | 4,58 |
| 21 | Wong et al., 1990, No. 1 | 400 | 20,00 | 800 | 38,0 | 423 | 3,20 | 300 | 1,42 | 0,19 | 394 | 461 | 6,61 |
| 22 | Wong et al., 1990, No. 2 | 400 | 18,00 | 800 | 37,0 | 475 | 3,20 | 340 | 0,47 | 0,39 | 412 | 489 | 3,96 |
| 23 | Lim et al., 1990, Con1 | 152 | 10,20 | 1140 | 34,5 | 448 | 5,57 | 620 | 1,45 | 0,24 | 22 | 14 | 4,63 |
| 24 | Lim et al., 1990, Con1 | 152 | 10,20 | 570 | 34,5 | 448 | 5,57 | 620 | 1,45 | 0,24 | 24 | 37 | 5,95 |
| 25 | Lim et al., 1990, Con1 | 152 | 10,20 | 570 | 34,5 | 448 | 5,57 | 620 | 1,45 | 0,35 | 24 | 36 | 5,23 |
| 26 | NIST, Full Scale Flexure | 1520 | 58,70 | 9140 | 35,8 | 475 | 1,99 | 493 | 0,63 | 0,07 | 13300 | 1289 | 5,41 |
| 27 | NIST, Full Scale Shear | 1520 | 60,30 | 4570 | 34,3 | 475 | 1,99 | 435 | 1,49 | 0,07 | 14500 | 2968 | 5,67 |
| 28 | NIST, Model N1 | 250 | 9,90 | 750 | 24,1 | 446 | 1,98 | 441 | 1,41 | 0,10 | 50 | 59 | 11,5 |
| 29 | NIST, Model N2 | 250 | 9,90 | 750 | 23,1 | 446 | 1,98 | 441 | 1,41 | 0,21 | 63 | 73 | 10,1 |
| 30 | NIST, Model N3 | 250 | 9,70 | 1500 | 25,4 | 446 | 1,98 | 476 | 0,68 | 0,10 | 57 | 32 | 6,09 |
| 31 | NIST, Model N4 | 250 | 9,90 | 750 | 24,4 | 446 | 1,98 | 441 | 1,41 | 0,10 | 51 | 63 | 9,98 |
| 32 | NIST, Model N5 | 250 | 9,90 | 750 | 24,3 | 446 | 1,98 | 441 | 1,41 | 0,20 | 64 | 77 | 10,3 |
| 33 | NIST, Model N6 | 250 | 9,70 | 1500 | 23,3 | 446 | 1,98 | 476 | 0,68 | 0,11 | 52 | 30 | 6,61 |
| 34 | Kunnath et al., 1997, A2 | 305 | 14,50 | 1372 | 29,0 | 448 | 2,04 | 434 | 0,94 | 0,09 | 115 | 74 | 5,89 |
| 35 | Kunnath et al., 1997, A6 | 305 | 14,50 | 1372 | 35,5 | 448 | 2,04 | 434 | 0,94 | 0,09 | 119 | 77 | 7,37 |
| 36 | Kunnath et al., 1997, A7 | 305 | 14,50 | 1372 | 32,8 | 448 | 2,04 | 434 | 0,94 | 0,09 | 120 | 79 | 10,1 |
| 37 | Kunnath et al., 1997, A8 | 305 | 14,50 | 1372 | 32,8 | 448 | 2,04 | 434 | 0,94 | 0,09 | 107 | 68 | 7,28 |
| 38 | Kunnath et al., 1997, A9 | 305 | 14,50 | 1372 | 32,5 | 448 | 2,04 | 434 | 0,94 | 0,09 | 114 | 75 | 9,11 |
| 39 | Kunnath et al., 1997, A10 | 305 | 14,50 | 1372 | 27,0 | 448 | 2,04 | 434 | 0,94 | 0,10 | 113 | 74 | 7,64 |
| 40 | Kunnath et al., 1997, A11 | 305 | 14,50 | 1372 | 27,0 | 448 | 2,04 | 434 | 0,94 | 0,10 | 103 | 68 | 7,66 |
| 41 | Kunnath et al., 1997, A12 | 305 | 14,50 | 1372 | 27,0 | 448 | 2,04 | 434 | 0,94 | 0,10 | 109 | 72 | 7,07 |
| 42 | Benzoni & Priestley 1994, NR1 | 610 | 15,88 | 914,5 | 30,0 | 462 | 0,52 | 361 | 0,28 | 0,06 | 365 | 393 | 14 |
| 43 | Benzoni & Priestley 1994, NR2 | 610 | 15,88 | 914,5 | 30,0 | 462 | 1,04 | 361 | 0,17 | 0,06 | 537 | 579 | 5,43 |
| 44 | Hose et al., 1997, SRPH1 | 610 | 27,76 | 3660 | 41,1 | 455 | 2,66 | 414 | 0,89 | 0,15 | 1300 | 285 | 6,47 |
| 45 | Vu et al., 1998, NH1 | 457 | 24,76 | 910 | 38,3 | 427,5 | 2,41 | 430,2 | 1,14 | 0,31 | 530 | 535 | 5,92 |
| 46 | Vu et al., 1998, NH3 | 457 | 24,76 | 910 | 39,4 | 427,5 | 2,41 | 430,2 | 1,14 | 0,15 | 501 | 510 | 7,49 |
| 47 | Vu et al., 1998, NH4 | 457 | 26,35 | 910 | 35,0 | 468,2 | 5,21 | 434,4 | 2,70 | 0,15 | 870 | 905 | 6,03 |
| 48 | Vu et al., 1998, NH5 | 457 | 24,76 | 910 | 35,2 | 507,5 | 2,41 | 448,2 | 0,85 | -0,08 | 344 | 403 | 7,00 |
| 49 | Vu et al., 1998, NH6 | 457 | 26,35 | 910 | 35,0 | 486,2 | 5,21 | 434,4 | 3,04 | 0,33 | 975 | 957 | 8,10 |
| 50 | Kowalsky et al., 1996, FL1 | 457 | 30,16 | 3656 | 36,6 | 477 | 3,62 | 445 | 0,92 | 0,30 | 544 | 101 | 6,95 |
| 51 | Kowalsky et al., 1996, FL2 | 457 | 30,16 | 3656 | 40,0 | 477 | 3,62 | 437 | 0,60 | 0,27 | 639 | 124 | 3,33 |
| 52 | Kowalsky et al., 1996, FL3 | 457 | 30,16 | 3656 | 38,6 | 477 | 3,62 | 445 | 0,92 | 0,28 | 611 | 117 | 5,84 |
| 53 | Lehman et al., 1998, 415 | 609,6 | 22,23 | 2438 | 31,0 | 461,96 | 1,49 | 606,76 | 0,70 | 0,07 | 708 | 269 | 7,51 |
| 54 | Lehman et al., 1998, 815 | 609,6 | 22,23 | 4876 | 31,0 | 461,96 | 1,49 | 606,76 | 0,70 | 0,07 | 745 | 130 | 5,62 |
| 55 | Lehman et al., 1998, 1015 | 609,6 | 22,23 | 6096 | 31,0 | 461,96 | 1,49 | 606,76 | 0,70 | 0,07 | 604 | 80 | 8,31 |
| 56 | Lehman et al., 1998, 407 | 609,6 | 22,23 | 2438 | 31,0 | 461,96 | 0,75 | 606,76 | 0,70 | 0,07 | 443 | 172 | 10,1 |
| 57 | Lehman et al., 1998, 430 | 609,6 | 22,23 | 2438 | 31,0 | 461,96 | 2,98 | 606,76 | 0,70 | 0,07 | 1180 | 448 | 5,70 |
| 58 | Calderone et al., 2000, 328 | 609,6 | 28,58 | 1828 | 34,5 | 441,28 | 2,73 | 606,76 | 0,89 | 0,09 | 1030 | 525 | 9,83 |
| 59 | Calderone et al., 2000, 828 | 609,6 | 28,58 | 4876 | 34,5 | 441,28 | 2,73 | 606,76 | 0,89 | 0,09 | 975 | 172 | 10,2 |
| 60 | Calderone et al., 2000, 1028 | 609,6 | 28,58 | 6096 | 34,5 | 441,28 | 2,73 | 606,76 | 0,89 | 0,09 | 1160 | 157 | 7,70 |
| 61 | Sritharan et al., 1996, IC1 | 600 | 30,16 | 1800 | 31,4 | 448 | 1,92 | 431 | 0,54 | 0,05 | 737 | 387 | 4,90 |
| 62 | Sritharan et al., 1996, IC2 | 600 | 30,16 | 1800 | 34,6 | 448 | 1,92 | 431 | 0,54 | 0,04 | 775 | 411 | 6,10 |
| 63 | Sritharan et al., 1996, IC3 | 600 | 30,16 | 1800 | 33,0 | 461 | 1,92 | 434 | 0,81 | 0,04 | 815 | 433 | 7,72 |

| | | | | | | | | | | | | | |
|----|-------------------------------|-------|---------|------|------|-------|------|--------|------|------|-----|-----|------|
| 64 | Saatcioglu & Baingo 1999, RC1 | 250 | 13,75 | 1645 | 65,0 | 419 | 3,28 | 1000 | 1,54 | 0,31 | 138 | 55 | 9,29 |
| 65 | Saatcioglu & Baingo 1999, RC3 | 250 | 13,75 | 1645 | 90,0 | 419 | 3,28 | 1000 | 1,54 | 0,42 | 163 | 56 | 5,25 |
| 66 | Saatcioglu & Baingo 1999, RC4 | 250 | 14,00 | 1645 | 90,0 | 419 | 3,28 | 580 | 1,75 | 0,42 | 162 | 55 | 3,66 |
| 67 | Saatcioglu & Baingo 1999, RC6 | 250 | 15,65 | 1645 | 90,0 | 419 | 3,28 | 420 | 1,74 | 0,42 | 154 | 57 | 5,51 |
| 68 | Saatcioglu & Baingo 1999, RC7 | 250 | 13,75 | 1645 | 90,0 | 419 | 3,28 | 1000 | 1,54 | 0,21 | 139 | 59 | 9,23 |
| 69 | Saatcioglu & Baingo 1999, RC8 | 250 | 13,75 | 1645 | 90,0 | 419 | 3,28 | 1000 | 1,54 | 0,42 | 158 | 55 | 3,68 |
| 70 | Saatcioglu & Baingo 1999, RC9 | 250 | 13,75 | 1645 | 90,0 | 419 | 3,28 | 420 | 3,43 | 0,42 | 200 | 71 | 10,2 |
| 71 | Nelson & Price 2000, Col 1 | 508 | 21,31 | 1524 | 56,2 | 470 | 0,99 | 455 | 0,13 | 0,13 | 488 | 283 | 4,50 |
| 72 | Nelson & Price 2000, Col 2 | 508 | 21,31 | 1524 | 56,3 | 470 | 0,99 | 455 | 0,13 | 0,11 | 456 | 279 | 5,17 |
| 73 | Nelson & Price 2000, Col 3 | 508 | 21,31 | 1524 | 57,0 | 470 | 0,99 | 455 | 0,13 | 0,10 | 423 | 260 | 5,51 |
| 74 | Nelson & Price 2000, Col 4 | 508 | 21,31 | 1524 | 52,7 | 470 | 0,99 | 455 | 0,13 | 0,11 | 415 | 252 | 6,97 |
| 75 | Henry 1998, 415p | 609,6 | 22,23 | 2438 | 37,2 | 462 | 1,49 | 606,76 | 0,70 | 0,12 | 831 | 277 | 4,41 |
| 76 | Henry 1998, 415s | 609,6 | 22,23 | 2438 | 37,2 | 462 | 1,49 | 606,76 | 0,35 | 0,06 | 716 | 259 | 5,86 |
| 77 | Chai, Priestley 1991, Test 3 | 609,6 | 20,00 | 3657 | 32,6 | 315,1 | 2,54 | 351,6 | 0,17 | 0,19 | 889 | 207 | 5,81 |
| 78 | Hamilton, 2002, UC11 | 406,4 | 14,9606 | 1854 | 36,5 | 458,5 | 1,17 | 691,5 | 0,53 | 0,00 | 130 | 70 | 6,59 |
| 79 | Hamilton, 2002, UC15 | 406,4 | 10,4394 | 1047 | 35,4 | 458,5 | 1,17 | 691,5 | 0,26 | 0,00 | 178 | 170 | 5,97 |

Appendix 2

Normalization of Data Set

| No | D | d' | L | f_c | f_y | ρ_l | f_{yw} | ρ_s | N/N _o | M _{max} | V _{max} | μ | Purpose of use |
|----|--------|--------|--------|--------|--------|----------|----------|----------|------------------|------------------|------------------|-----------|----------------|
| 1 | 0,1813 | 0,1640 | 0,0268 | 0,2152 | 0,6619 | 0,5307 | 0,0400 | 0,1152 | 0,1600 | 0,016162 | 0,103927 | 0,045277 | Training |
| 2 | 0,1813 | 0,1640 | 0,0268 | 0,2108 | 0,0000 | 0,5307 | 0,0400 | 0,1152 | 0,1600 | 0,010568 | 0,069397 | 0,355972 | Training |
| 3 | 0,1813 | 0,2036 | 0,0268 | 0,1121 | 0,6619 | 0,5307 | 0,0229 | 0,1152 | 0,1600 | 0,014436 | 0,093094 | 0,053084 | Test |
| 4 | 0,1813 | 0,1640 | 0,0268 | 0,1196 | 0,6619 | 0,5307 | 0,0400 | 0,1909 | 0,1600 | 0,016784 | 0,107312 | 0,02498 | Training |
| 5 | 0,1813 | 0,1640 | 0,0035 | 0,1046 | 0,6619 | 0,5307 | 0,0400 | 0,1152 | 0,1600 | 0,014712 | 0,127962 | 0,001561 | Test |
| 6 | 0,1813 | 0,1640 | 0,0268 | 0,0957 | 0,7187 | 0,5307 | 0,1029 | 0,0758 | 0,1600 | 0,014021 | 0,090386 | 0 | Training |
| 7 | 0,1813 | 0,1640 | 0,0268 | 0,0837 | 0,7187 | 0,5307 | 0,1029 | 0,2697 | 0,5600 | 0,02452 | 0,145904 | 0,120219 | Test |
| 8 | 0,1813 | 0,1640 | 0,0502 | 0,1016 | 0,7187 | 0,5307 | 0,1029 | 0,2697 | 0,5600 | 0,026178 | 0,118483 | 0,164715 | Training |
| 9 | 0,1813 | 0,2233 | 0,0268 | 0,1211 | 0,7187 | 0,5307 | 0,0457 | 0,2697 | 0,5600 | 0,024106 | 0,143196 | 0,081967 | Training |
| 10 | 0,1813 | 0,1640 | 0,0035 | 0,0822 | 0,6619 | 0,5307 | 0,0400 | 0,2697 | 0,3600 | 0,020652 | 0,173324 | 0 | Training |
| 11 | 0,1813 | 0,1640 | 0,0268 | 0,1958 | 0,6619 | 0,5307 | 0,0371 | 0,2697 | 0,3600 | 0,023691 | 0,142857 | 0,250585 | Test |
| 12 | 0,1813 | 0,1640 | 0,0268 | 0,1584 | 0,6052 | 0,5386 | 0,0371 | 0,1152 | 0,1600 | 0,015955 | 0,102234 | 0,176425 | Training |
| 13 | 0,1813 | 0,1640 | 0,0268 | 0,1749 | 0,6619 | 0,2772 | 0,0371 | 0,1152 | 0,1600 | 0,011189 | 0,073121 | 0,380172 | Training |
| 14 | 0,1813 | 0,1640 | 0,0268 | 0,1540 | 0,6619 | 0,5307 | 0,0371 | 0,1152 | 0,3600 | 0,018304 | 0,114421 | 0,062451 | Training |
| 15 | 0,1813 | 0,1640 | 0,0502 | 0,1674 | 0,6619 | 0,5307 | 0,0371 | 0,1152 | 0,3600 | 0,020583 | 0,10088 | 0,136612 | Test |
| 16 | 0,1813 | 0,1640 | 0,0035 | 0,1779 | 0,6619 | 0,5307 | 0,0371 | 0,1152 | 0,3600 | 0,019823 | 0,166215 | 0,082748 | Training |
| 17 | 0,1813 | 0,1640 | 0,0035 | 0,1689 | 0,6619 | 0,5307 | 0,0371 | 0,0758 | 0,3600 | 0,016853 | 0,143196 | 0,046838 | Test |
| 19 | 0,1813 | 0,2233 | 0,0268 | 0,1375 | 0,6619 | 0,5307 | 0,0457 | 0,1909 | 0,1600 | 0,014228 | 0,09174 | 0,131148 | Training |
| 20 | 0,1813 | 0,2036 | 0,0268 | 0,1495 | 0,6619 | 0,5307 | 0,0143 | 0,1939 | 0,1600 | 0,016853 | 0,107989 | 0,256831 | Test |
| 21 | 0,1813 | 0,2036 | 0,0268 | 0,2227 | 0,6005 | 0,5307 | 0,0000 | 0,3909 | 0,5400 | 0,017268 | 0,110697 | 0,261514 | Training |
| 22 | 0,1813 | 0,1640 | 0,0268 | 0,2078 | 0,8463 | 0,5307 | 0,0571 | 0,1030 | 0,9400 | 0,025694 | 0,15132 | 0,419984 | Training |
| 23 | 0,0000 | 0,0099 | 0,0665 | 0,1704 | 0,7187 | 1,0000 | 0,4571 | 0,4000 | 0,6400 | 0,026937 | 0,160799 | 0,213115 | Training |
| 24 | 0,0000 | 0,0099 | 0,0000 | 0,1704 | 0,7187 | 1,0000 | 0,4571 | 0,4000 | 0,6400 | 0 | 0 | 0,265418 | Training |
| 25 | 0,0000 | 0,0099 | 0,0000 | 0,1704 | 0,7187 | 1,0000 | 0,4571 | 0,4000 | 0,8600 | 0,000138 | 0,007786 | 0,368462 | Test |
| 26 | 1,0000 | 0,9684 | 1,0000 | 0,1898 | 0,8463 | 0,2911 | 0,2757 | 0,1515 | 0,3000 | 0,000138 | 0,007448 | 0,312256 | Training |
| 27 | 1,0000 | 1,0000 | 0,4667 | 0,1674 | 0,8463 | 0,2911 | 0,1929 | 0,4121 | 0,3000 | 0,917116 | 0,431618 | 0,326308 | Training |
| 28 | 0,0716 | 0,0040 | 0,0210 | 0,0149 | 0,7092 | 0,2891 | 0,2014 | 0,3879 | 0,3600 | 1 | 1 | 0,346604 | Training |
| 29 | 0,0716 | 0,0040 | 0,0210 | 0,0000 | 0,7092 | 0,2891 | 0,2014 | 0,3879 | 0,5800 | 0,001934 | 0,015234 | 0,806401 | Test |
| 30 | 0,0716 | 0,0000 | 0,1085 | 0,0344 | 0,7092 | 0,2891 | 0,2514 | 0,1667 | 0,3600 | 0,002832 | 0,019973 | 0,692428 | Training |
| 31 | 0,0716 | 0,0040 | 0,0210 | 0,0194 | 0,7092 | 0,2891 | 0,2014 | 0,3879 | 0,3600 | 0,002417 | 0,006093 | 0,379391 | Test |
| 32 | 0,0716 | 0,0040 | 0,0210 | 0,0179 | 0,7092 | 0,2891 | 0,2014 | 0,3879 | 0,5600 | 0,002003 | 0,016588 | 0,68306 | Training |
| 33 | 0,0716 | 0,0000 | 0,1085 | 0,0030 | 0,7092 | 0,2891 | 0,2514 | 0,1667 | 0,3800 | 0,002901 | 0,021327 | 0,714286 | Test |
| 34 | 0,1118 | 0,0949 | 0,0936 | 0,0882 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3400 | 0,002072 | 0,005416 | 0,4119984 | Training |
| 35 | 0,1118 | 0,0949 | 0,0936 | 0,1854 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3400 | 0,006424 | 0,020311 | 0,363778 | Test |
| 36 | 0,1118 | 0,0949 | 0,0936 | 0,1450 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3400 | 0,0067 | 0,021327 | 0,479313 | Training |
| 37 | 0,1118 | 0,0949 | 0,0936 | 0,1450 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3400 | 0,006769 | 0,022004 | 0,693208 | Test |
| 38 | 0,1118 | 0,0949 | 0,0936 | 0,1405 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3400 | 0,005871 | 0,01828 | 0,472287 | Training |
| 39 | 0,1118 | 0,0949 | 0,0936 | 0,0583 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3600 | 0,006354 | 0,02065 | 0,615144 | Test |
| 40 | 0,1118 | 0,0949 | 0,0936 | 0,0583 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3600 | 0,006285 | 0,020311 | 0,50039 | Training |
| 41 | 0,1118 | 0,0949 | 0,0936 | 0,0583 | 0,7187 | 0,3010 | 0,1914 | 0,2455 | 0,3600 | 0,005595 | 0,01828 | 0,501952 | Test |
| 42 | 0,3348 | 0,1221 | 0,0402 | 0,1031 | 0,7849 | 0,0000 | 0,0871 | 0,0455 | 0,2800 | 0,006009 | 0,019634 | 0,455894 | Training |
| 43 | 0,3348 | 0,1221 | 0,0402 | 0,1031 | 0,7849 | 0,1030 | 0,0871 | 0,0121 | 0,2800 | 0,023691 | 0,128301 | 1 | Test |
| 44 | 0,3348 | 0,3569 | 0,3606 | 0,2691 | 0,7518 | 0,4238 | 0,1629 | 0,2303 | 0,4600 | 0,035571 | 0,191266 | 0,327869 | Training |
| 45 | 0,2230 | 0,2976 | 0,0397 | 0,2272 | 0,6217 | 0,3743 | 0,1860 | 0,3061 | 0,7800 | 0,088272 | 0,09174 | 0,409055 | Test |
| 46 | 0,2230 | 0,2976 | 0,0397 | 0,2436 | 0,6217 | 0,3743 | 0,1860 | 0,3061 | 0,4600 | 0,035088 | 0,176371 | 0,36612 | Training |
| 47 | 0,2230 | 0,3291 | 0,0397 | 0,1779 | 0,8142 | 0,9287 | 0,1920 | 0,7788 | 0,4600 | 0,033085 | 0,167908 | 0,488681 | Training |
| 48 | 0,2230 | 0,2976 | 0,0397 | 0,1809 | 1,0000 | 0,3743 | 0,2117 | 0,2182 | 0,0000 | 0,058572 | 0,301625 | 0,374707 | Training |
| 49 | 0,2230 | 0,3291 | 0,0397 | 0,1779 | 0,8993 | 0,9287 | 0,1920 | 0,8818 | 0,8200 | 0,022241 | 0,131686 | 0,450429 | Training |

| | | | | | | | | | | | | | |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|----------|----------|----------|
| 50 | 0,2230 | 0,4043 | 0,3601 | 0,2018 | 0,8558 | 0,6139 | 0,2071 | 0,2394 | 0,7600 | 0,065824 | 0,319228 | 0,5363 | Test |
| 51 | 0,2230 | 0,4043 | 0,3601 | 0,2526 | 0,8558 | 0,6139 | 0,1957 | 0,1424 | 0,7000 | 0,036055 | 0,029452 | 0,446526 | Training |
| 52 | 0,2230 | 0,4043 | 0,3601 | 0,2317 | 0,8558 | 0,6139 | 0,2071 | 0,2394 | 0,7200 | 0,042616 | 0,037238 | 0,163934 | Test |
| 53 | 0,3345 | 0,2476 | 0,2180 | 0,1181 | 0,7847 | 0,1921 | 0,4382 | 0,1727 | 0,3000 | 0,040682 | 0,034868 | 0,359875 | Training |
| 54 | 0,3345 | 0,2476 | 0,5025 | 0,1181 | 0,7847 | 0,1921 | 0,4382 | 0,1727 | 0,3000 | 0,049938 | 0,039269 | 0,342701 | Training |
| 55 | 0,3345 | 0,2476 | 0,6448 | 0,1181 | 0,7847 | 0,1921 | 0,4382 | 0,1727 | 0,3000 | 0,040199 | 0,022343 | 0,552693 | Test |
| 56 | 0,3345 | 0,2476 | 0,2180 | 0,1181 | 0,7847 | 0,0455 | 0,4382 | 0,1727 | 0,3000 | 0,029079 | 0,053487 | 0,693208 | Training |
| 57 | 0,3345 | 0,2476 | 0,2180 | 0,1181 | 0,7847 | 0,4871 | 0,4382 | 0,1727 | 0,3000 | 0,079983 | 0,146919 | 0,348946 | Training |
| 58 | 0,3345 | 0,3731 | 0,1469 | 0,1704 | 0,6869 | 0,4376 | 0,4382 | 0,2303 | 0,3400 | 0,069623 | 0,172986 | 0,671351 | Training |
| 59 | 0,3345 | 0,3731 | 0,5025 | 0,1704 | 0,6869 | 0,4376 | 0,4382 | 0,2303 | 0,3400 | 0,065824 | 0,053487 | 0,700234 | Test |
| 60 | 0,3345 | 0,3731 | 0,6448 | 0,1704 | 0,6869 | 0,4376 | 0,4382 | 0,2303 | 0,3400 | 0,078602 | 0,048409 | 0,505074 | Training |
| 61 | 0,3275 | 0,4043 | 0,1435 | 0,1241 | 0,7187 | 0,2772 | 0,1871 | 0,1242 | 0,2600 | 0,049385 | 0,126269 | 0,286495 | Test |
| 62 | 0,3275 | 0,4043 | 0,1435 | 0,1719 | 0,7187 | 0,2772 | 0,1871 | 0,1242 | 0,2400 | 0,05201 | 0,134394 | 0,380172 | Training |
| 63 | 0,3275 | 0,4043 | 0,1435 | 0,1480 | 0,7801 | 0,2772 | 0,1914 | 0,2061 | 0,2400 | 0,054773 | 0,141842 | 0,506635 | Test |
| 64 | 0,0716 | 0,0800 | 0,1254 | 0,6263 | 0,5816 | 0,5465 | 1,0000 | 0,4273 | 0,7800 | 0,008012 | 0,013879 | 0,629196 | Training |
| 65 | 0,0716 | 0,0800 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 1,0000 | 0,4273 | 1,0000 | 0,009739 | 0,014218 | 0,313817 | Training |
| 66 | 0,0716 | 0,0850 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 0,4000 | 0,4909 | 1,0000 | 0,00967 | 0,013879 | 0,189696 | Training |
| 67 | 0,0716 | 0,1176 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 0,1714 | 0,4879 | 1,0000 | 0,009117 | 0,014557 | 0,334114 | Training |
| 68 | 0,0716 | 0,0800 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 1,0000 | 0,4273 | 0,5800 | 0,008081 | 0,015234 | 0,624512 | Test |
| 69 | 0,0716 | 0,0800 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 1,0000 | 0,4273 | 1,0000 | 0,009394 | 0,013879 | 0,191257 | Training |
| 70 | 0,0716 | 0,0800 | 0,1254 | 1,0000 | 0,5816 | 0,5465 | 0,1714 | 1,0000 | 1,0000 | 0,012295 | 0,019296 | 0,705699 | Test |
| 71 | 0,2602 | 0,2294 | 0,1113 | 0,4948 | 0,8227 | 0,0931 | 0,2214 | 0,0000 | 0,4200 | 0,032187 | 0,091063 | 0,255269 | Training |
| 72 | 0,2602 | 0,2294 | 0,1113 | 0,4963 | 0,8227 | 0,0931 | 0,2214 | 0,0000 | 0,3800 | 0,029977 | 0,089709 | 0,307572 | Test |
| 73 | 0,2602 | 0,2294 | 0,1113 | 0,5067 | 0,8227 | 0,0931 | 0,2214 | 0,0000 | 0,3600 | 0,027697 | 0,083277 | 0,334114 | Training |
| 74 | 0,2602 | 0,2294 | 0,1113 | 0,4425 | 0,8227 | 0,0931 | 0,2214 | 0,0000 | 0,3800 | 0,027145 | 0,080569 | 0,448087 | Test |
| 75 | 0,3345 | 0,2476 | 0,2180 | 0,2108 | 0,7849 | 0,1921 | 0,4382 | 0,1727 | 0,4000 | 0,055878 | 0,089032 | 0,248244 | Training |
| 76 | 0,3345 | 0,2476 | 0,2180 | 0,2108 | 0,7849 | 0,1921 | 0,4382 | 0,0667 | 0,2800 | 0,047935 | 0,082938 | 0,361436 | Test |
| 77 | 0,3345 | 0,2036 | 0,3602 | 0,1420 | 0,0903 | 0,4000 | 0,0737 | 0,0121 | 0,5400 | 0,059884 | 0,065335 | 0,357533 | Training |
| 78 | 0,1860 | 0,1040 | 0,1498 | 0,2003 | 0,7683 | 0,1287 | 0,5593 | 0,1212 | 0,1600 | 0,00746 | 0,018957 | 0,418423 | Training |
| 79 | 0,1860 | 0,0146 | 0,0557 | 0,1839 | 0,7683 | 0,1287 | 0,5593 | 0,0394 | 0,1600 | 0,010775 | 0,05281 | 0,370023 | Training |

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